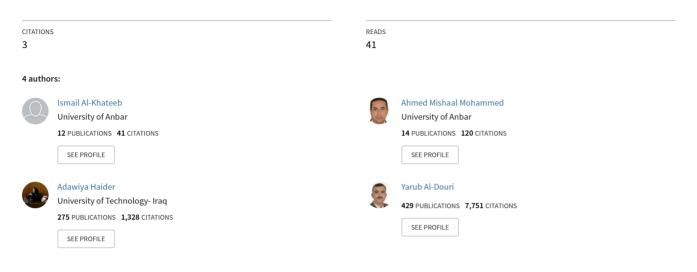
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## Removal of Benzene from Aqueous Solution Using Carbon Nanotube Synthesized from Fuel Oil Waste

#### Article in Advanced Materials Research · April 2014

DOI: 10.4028/www.scientific.net/AMR.925.105



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# Removal of benzene from aqueous solution using carbon nanotube synthesized from fuel oil waste

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#### Keywords: CNT; Benzene; Fuel oil; Adsorption

#### Abstract:

This investigation is dealing with adsorption of benzene compound from aqueous solution using a new carbon nanotube (CNT) synthesized from a fuel oil waste of power plants which identify by FE-SEM and TEM. It was found that a CNT has a very significant adsorption for benzene compared to that of non-activated carbon. The equilibrium adsorption data were analyzed using adsorption models of Langmuir, Freundlich and Temkin. The results showed that the model isotherms are fitting very well with the experimental data. Kinetic study was conducted and the results pointed out that a pseudo-first order model was represented the data. Values of the activation thermodynamic functions were calculated through equilibrium constants at different temperature. All values of Gibbs functions were negative with values of -1.6 and -13.0 kJmol<sup>-1</sup> for non-active and CNT respectively, while values of enthalpy and entropy were about -33kJmol<sup>-1</sup> and-65JK<sup>-1</sup> mol<sup>-1</sup> for CNT respectively. These results indicated that the adsorption process was feasible, spontaneous and exothermic.

## **1.Introduction**

Carbon nanotubes have different characteristics of that of the macro-scale. Uses of carbon nanotubes are concern mostly on environmental aspects as unique sorbents for removal of pollutants [1-3]. Adsorption technology has been used widely for a removal of organic compounds from aqueous solution using activated and nanocarbon materials [4-6]. However, the removal of benzene has been investigated with highly significant approach using carbon nanotubes [1,2,7], graphitized carbon [8], carbon nano porous coated with polymers [4]. The main objective of this research is to remove the residual benzene using synthetic CNT manufactured from fuel oil wastes as the adsorbent.

## 2. Experimental

The samples of fuel oil residue were collected from the power plant in Al-Anbar area, Iraq, and refining according to the procedure mentioned elsewhere [9].

The CNT was synthesis from fuel oil waste using ultrasonic technology and identified using FE-SEM and TEM as shown in Figs. (1) and (2) [10].

## 2.1. Characterization

Surface area, density, ash content, pH and Moisture content of prepared CNT were determined as shown in table (1).

Samples	Surface area m <sup>2</sup> /g	Density g/cm <sup>3</sup>	Ash%	рН	Moisture %
CNT	1050.4	0.4908	0.11	3.79	1.600
Non-active carbon	72.32	0.5834	2.61	6.15	0.773

Table1: Characteristics of CNT and non-activated carbon samples.

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## 2.2. Adsorption studies

Determination of equilibration time for benzene adsorption on CNT was done by shaking 5ml of benzene at concentrations of 50,200 and 300 ppm with 0.1gof adsorbate at constant temperature of 283,293,313 and 333 K for 120 min. Sub-sample were taken from each concentration at 10 to 120 min for kinetic studies and then filtrated. UV-Vis spectrophotometer has been used to measure the absorbance for benzene at equilibrated solutions at certain wavelength (204 nm). The quantity of adsorbate was calculated by using the following formula:

 $q_e = V_{Sol} (C_o - C_e)/M$ 

(1)

(2)

Where  $q_e$  is quantity of adsorbate (mg/g),  $V_{Sol}$  is total volume of adsorbate solution (L),  $C_o$  is initial concentration of adsorbate solution (mg/L),  $C_e$  is concentration of adsorbate solution at equilibrium (mg/L) and M is weight of adsorbate (g). While the removal percentage of benzene and equilibrium adsorption  $q_e$  (mg/g) was uptake, using the formula 2.

% adsorption Efficiency =  $(C_o - C_e)/C_o \times 100$ 

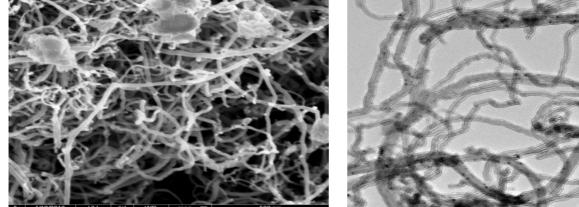


Fig.1: FE-SEM image of CNT

## Fig.2: TEM image of CNT

## 3. Results and Discussions

## 3.1. Adsorption Equilibrium

The isotherm of the benzene adsorption by synthetic CNT was represented by applying the Langmuir, Freundlich and Temkin adsorption models, and it was found that the adsorption process on the synthetic CNT fits very well with the isotherm models table (2). The Freundlich linear isotherm is expressed as:

$$Log Q_e = log K_f + 1/n log C_e$$

(3)

Where  $Q_e$  is the equilibrium value of benzene adsorbed per unit weight of synthetic CNT powder, i.e. a liquid-phase sorbate concentration occurred at equilibrium and  $K_f$  as the Freundlich constant. Freundlich constants are shown in table (2) while the relations are clearly indicated that the Freundlich isotherm model fits the analyzed data according to its correlation coefficients ( $R^2$ ).

The synthetic CNT powder takes up benzene on a heterogeneous surface by multilayer adsorption as described by Langmuir. However, the Langmuir linear isotherm is expressed as  $C_e/Q_e = (1/K_L Q_o) + (1/Q_o) Ce$  (4)

Where  $Q_o$  is the maximum amount of adsorption corresponding to complete monolayer coverage and  $K_L$  is the Langmuir constant. Table (2) shows the Langmuir factors and relations.

The linear form of Temkin isotherm is expressed as:

 $q_e = B \ln A + B \ln C_e$ 

Table (2) shows the Temkin factors and relations.

		ТК	Langmuir constants			Freu	ndlich co	onstants	Temkin constants		
		IK	$\mathbf{R}^2$	a	KL	$\mathbf{R}^2$	n	K <sub>F</sub>	$\mathbb{R}^2$	В	А
CNT		283	0.980	9.667	111.11	0.935	5.587	9.506	0.924	1.760	245.25
C		293	0.935	2.399	28.571	0.981	2.222	5.916	0.974	4.899	2.463
		313	0.956	3.423	38.461	0.992	2.012	4.989	0.916	1.850	67.12
		333	0.948	2.256	25.641	0.985	1.767	4.335	0.986	5.662	1.357
0		283	0.806	- 0.013	0.016	0.976	0.337	2.68×10 <sup>-5</sup>	0.868	9.463	0.031
Non-active carbon		293	0.795	- 0.012	0.014	0.984	0.325	1.44×10 <sup>-5</sup>	0.913	9.509	0.029
on-		313	0.580	- 0.013	0.007	0.907	0.237	8.9×10 <sup>-8</sup>	0.960	11.626	0.024
~		333	0.385	- 0.013	0.002	0.802	0.165	2.917×10 <sup>-11</sup>	0.931	13.718	0.022

Table 2: The values of Langmuir, Freundlich and Temkin constants at different temperatures.

The adsorption rate of benzene increased with benzene concentration and decreased with temperature. (Tables 3, and 4). A complete removal of benzene concentration was obtained for initial concentration of 50 ppm and temperature of 283 K. Hence it is clearly proved that benzene adsorption by synthetic CNT agrees fair enough with the Langmuir, Freundlich and Temkin adsorption models. It was poorly fit with Langmuir isotherm model using non-active carbon. The correlation coefficient was very high throughout the experimental range of benzene concentrations studied.

Table3: The adsorption percentage of benzene at concentration 50 mg/L for different temperature.

_		adsorption efficiency %										
Temp.	283K		293K		313K		333K					
Time	CNT	Non-active carbon	CNT	Non-active carbon	CNT	Non-active carbon	CNT	Non-active carbon				
0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00				
10	90.74	3.88	90.33	2.87	89.67	1.68	84.55	0.49				
20	91.53	6.42	90.74	5.92	90.51	4.90	87.67	1.34				
30	93.26	7.10	92.09	6.42	91.67	5.58	89.81	1.68				
40	93.95	8.12	93.63	7.78	93.44	6.42	92.74	1.85				
50	96.33	12.45	95.72	11.00	95.40	8.80	95.07	2.19				
60	98.14	17.78	97.67	14.90	96.65	9.14	96.33	2.53				
70	99.02	24.90	98.56	21.34	97.49	16.59	97.02	2.70				
80	99.63	34.90	99.44	32.36	98.05	17.44	97.58	3.03				
90	99.91	35.24	99.81	32.53	99.63	17.44	97.86	3.54				
100	100.00	36.09	100.00	32.53	100.00	17.61	99.21	4.73				
110	100.00	36.09	100.00	32.70	100.00	18.29	100.00	5.07				
120	100.00	36.09	100.00	32.70	100.00	18.29	100.00	5.41				

Table 4: The adsorption percentage of benzene at concentration 300 mg/L for different temperatures.

	adsorption efficiency %									
Temp.	283K		293K		31	13K	333K			
Time	CNT	Non-active carbon	CNT Non-active carbon		CNT	Non-active carbon	CNT	Non-active carbon		
0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		
10	95.03	69.46	88.97	69.29	87.24	65.62	81.52	62.09		
20	95.73	70.96	91.49	70.03	90.18	68.78	85.58	66.75		
30	95.86	71.13	92.03	70.65	91.52	70.51	87.06	69.69		
40	95.97	74.43	93.00	71.44	92.49	71.33	88.49	71.01		
50	97.73	74.74	94.18	71.86	93.49	71.47	90.27	71.35		
60	97.93	75.17	95.03	72.71	94.12	72.20	90.85	71.75		
70	98.17	76.10	95.79	73.02	94.49	72.77	92.24	72.00		
80	98.42	76.38	96.36	73.36	95.30	72.79	93.30	72.65		
90	98.55	76.58	98.05	73.50	96.36	72.91	94.76	72.94		
100	98.79	76.58	98.19	73.56	97.45	73.05	95.64	72.99		
110	98.98	76.58	98.33	73.61	97.89	73.08	97.79	73.02		
120	99.09	76.64	98.45	73.61	98.17	73.10	98.11	73.05		

#### **3.2.** Thermodynamic parameters

The thermodynamic parameters  $\Delta G^{\circ}$ ,  $\Delta S^{\circ}$ , and  $\Delta H^{\circ}$  for adsorption processes are determined by using following equations [11].

## $\Delta G^{o} = -RT \ln K$

Where K is the thermodynamic equilibrium constant. The effect of temperature on thermodynamic constant is determined by:

 $Log K = \Delta S^{o} / 2.303 R - \Delta H^{o} / 2.303 RT$ 

Where  $\Delta G^{\circ}$  is the free energy change (kJ/mol); R is the universal constant (8.314 J/mol K) and T the absolute temperature (K);  $\Delta H^{\circ}$  change in enthalpy;  $\Delta S^{\circ}$  is the change in entropy. The  $\Delta H^{\circ}$  and  $\Delta S^{\circ}$  values were calculated from slope and intercept of the linear plot, of log K vs. 1/T as shown in Fig. (3). The corresponding values of thermodynamic parameters are presented in Table 5. The negative values of  $\Delta G^{\circ}$  indicate that the benzene adsorption process is spontaneous and feasible. The negative value of  $\Delta H^{\circ}$  shown the adsorption process is exothermic in nature. The negative  $\Delta S^{\circ}$  indicated the decrease in randomness at the solid-liquid interface during adsorption of benzene on carbon.

Samples	Initial Conc.(mg/l)	T(K)	K	ΔH° kJ.mol <sup>-1</sup>	ΔS° J.mol <sup>-1</sup> .k <sup>-1</sup>	ΔG° kJ.mol <sup>-1</sup>
	200	283	572.066		-64.343	-14.939
٧T	200	293	270.396	-33.148	-66.577	-13.641
5	200	313	99.770		-67.636	-11.978
	200	333	69.497		-64.282	-11.742
9	200	283	2.065		-3.088	-1.706
bon	200	293	2.002	2 580	-3.037	-1.690
Non-active carbon	200	313	1.906	-2.580	-2.881	-1.678
2 2	200	333	1.744		-3.123	-1.540

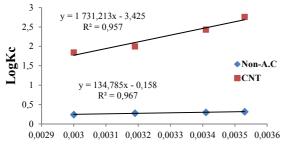
Table 5: Thermodynamic functions of benzene adsorption process.

## **3.3.** Adsorption kinetics

The adsorption data of benzene by CNT was fitted through kinetic model including pseudo-first order kinetic [12] as shown in following equation.

 $Ln (q_e-q_t) = lnq_e-k_1t$ 

Where  $q_e (mg/g)$  is the amount of benzene at equilibrium time while  $q_t (mg/g)$  is the amount of benzene at any time (t), k (min<sup>-1</sup>) is the pseudo-first order rate constant k and  $q_e$  were determined from the slope and intercept of the linear plot of ln ( $q_e$ - $q_t$ ) against t, respectively Fig. 4.



1/T (K<sup>-1</sup>)

Fig. 3: The plot of Log Kc vs. 1/T with CNT and Non-active carbon

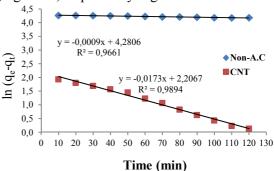


Fig.4: Relationship between Ln (Ce) and Time for benzene solutions at temperature of 283K and Conc. (200mg/L) for CNT and Non- active carbon.

## 4. Conclusions

The addition of CNT powder as an absorbent to a sample of benzene reduces, the concentration dramatically. About 100% reduction in concentration of benzene was obtained. The adsorption process of CNT powder fit the Langmuir, Freundlich and Temkin isotherm equilibrium adsorption models.

(6)

(8)

(7)

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10.4028/www.scientific.net/AMR.925

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